

Measurements of the non-uniformities seeded by NIF ignition capsule ablator materials

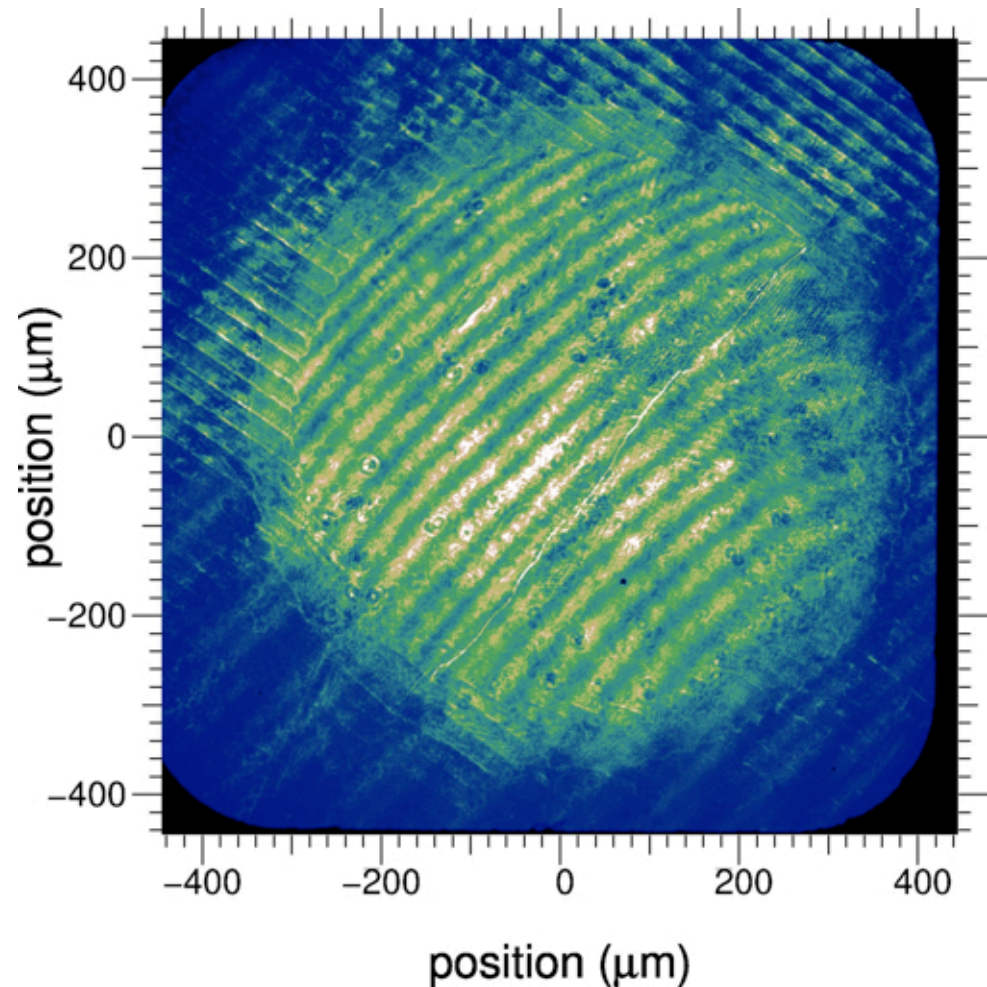
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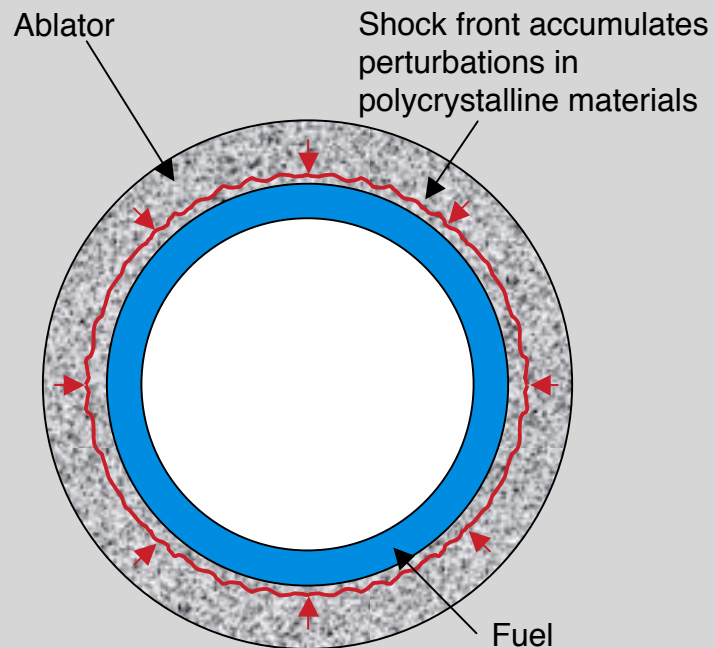


Summary

- **Characterization of ablator non-uniformities at the seed level during the first shock stage requires ultra-high sensitivity velocimetry**
- **A high resolution two-dimensional imaging VISAR has been built and fielded at OMEGA**
- **Tests on NIF ablator materials have begun**
- **Preliminary results (qualitative):**
 - **Non-uniformities seeded by Be(1%Cu) samples appear to be at levels near the detection limit of the interferometer**
 - **The level of non-uniformities seeded by diamond ablators is higher**
 - **Data analysis is ongoing**

Direct characterization of seed-level non-uniformities during the first shock stage requires a high sensitivity measurement

Goal: characterize non-uniformities at the seed level



Capsules are predicted to remain stable if the level of velocity non-uniformities is $< \text{few parts in } 10^4$

Requirements to detect seed-level non-uniformities

- Flow non-uniformities $\sim 1 \text{ m/s}$ within a flow field moving at $\sim 10 \text{ km/s}$ (velocity resolution at 1 part in 10^4)
- High spatial resolution ($\leq 5 \mu\text{m}$)
 - Be grain size $\sim 10 \mu\text{m}$
 - HDC grain size $\sim 200 \text{ nm}$
- Two-dimensional time-resolved snapshot to identify dominant modes & scale lengths

Current line-VISAR capabilities (e.g. at NIF and OMEGA) are not adequate for this measurement

Concept: detect non-uniformities in the shock just after it transits the ablator

Estimated ripple amplitude corresponding to NIF uniformity specification

Ripple oscillation time:

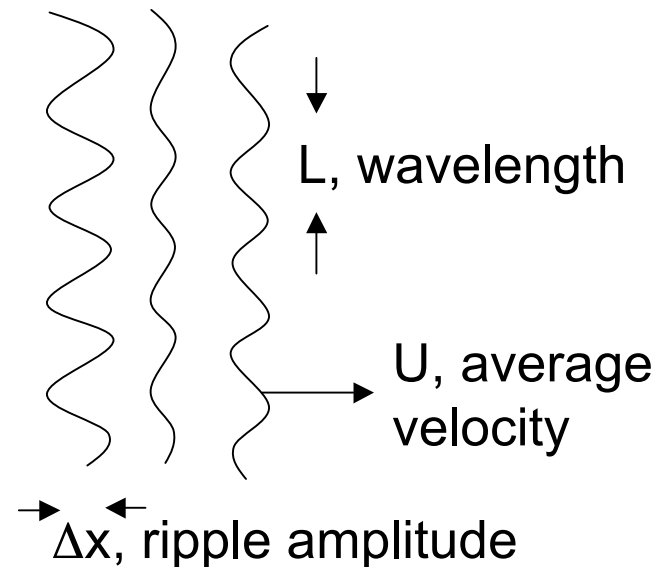
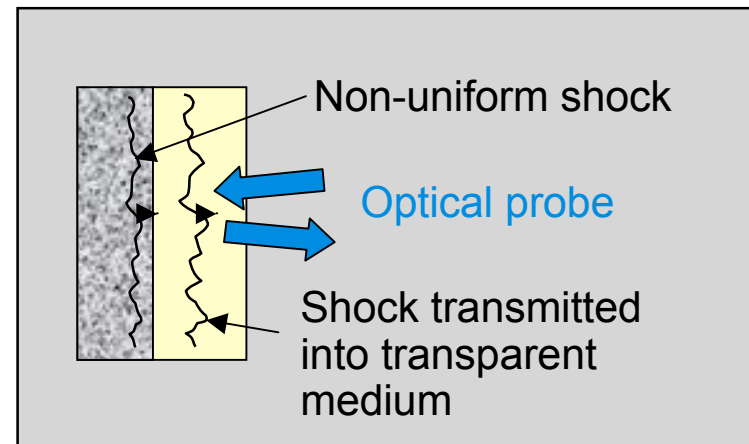
$$\Delta t \sim L/U$$

Ripple amplitude for current NIF designs:

$$\Delta x = \Delta U \Delta t = \Delta U/U L = 10^{-4} L$$

For ripple wavelengths near $L \sim 2 \mu\text{m}$, our resolution limit, the NIF ripple amplitude is $\Delta x \sim 0.2 \text{ nm}$.

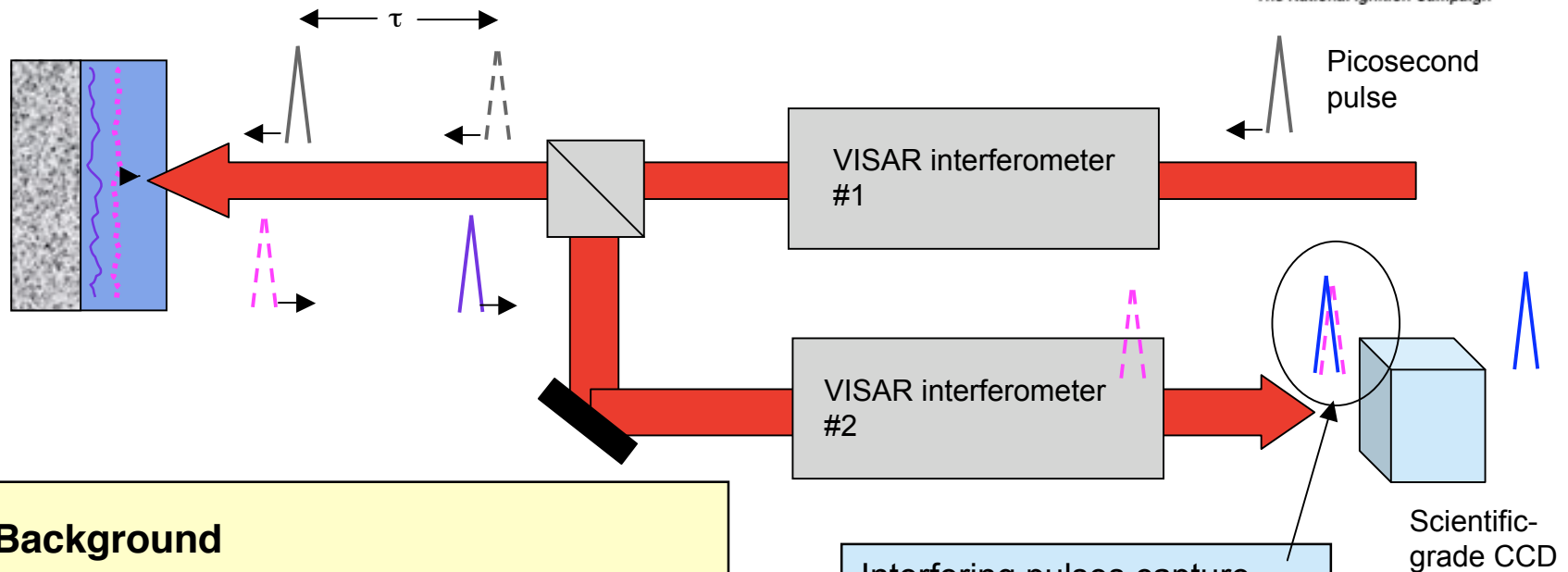
For a $\lambda = 400 \text{ nm}$ probe wavelength this is equivalent to $\sim \lambda/2000$ or $\sim 3 \text{ mrad}$



Two-dimensional VISAR with picosecond pulse illumination



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Background

- Scheme is a variation on a *white light VISAR**
- Uses quadrature readout for high accuracy phase extraction
- New content
 - Picosecond pulse illumination
 - High dynamic range scientific-grade-CCD detection
 - Two-dimensional velocity field

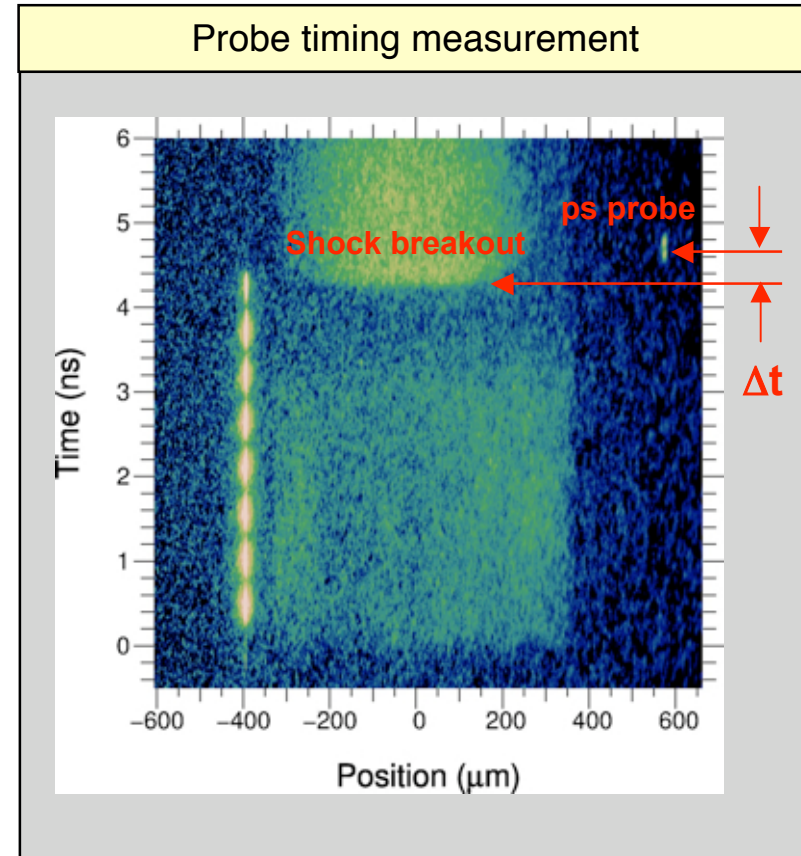
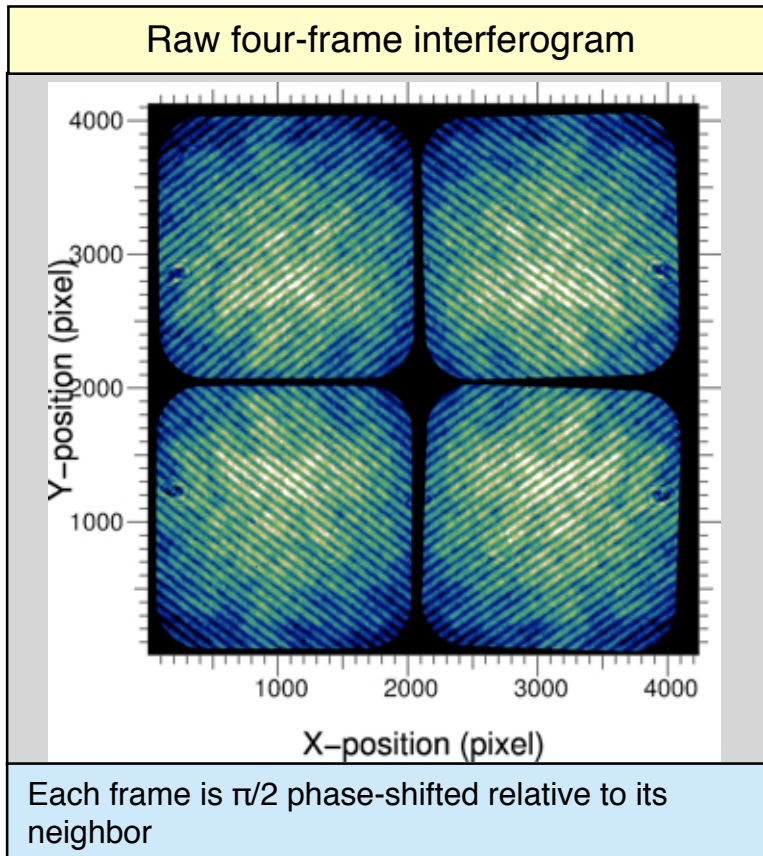
Interfering pulses capture *changes* in the shock front surface topology that have taken place during the delay interval τ .

Previous literature

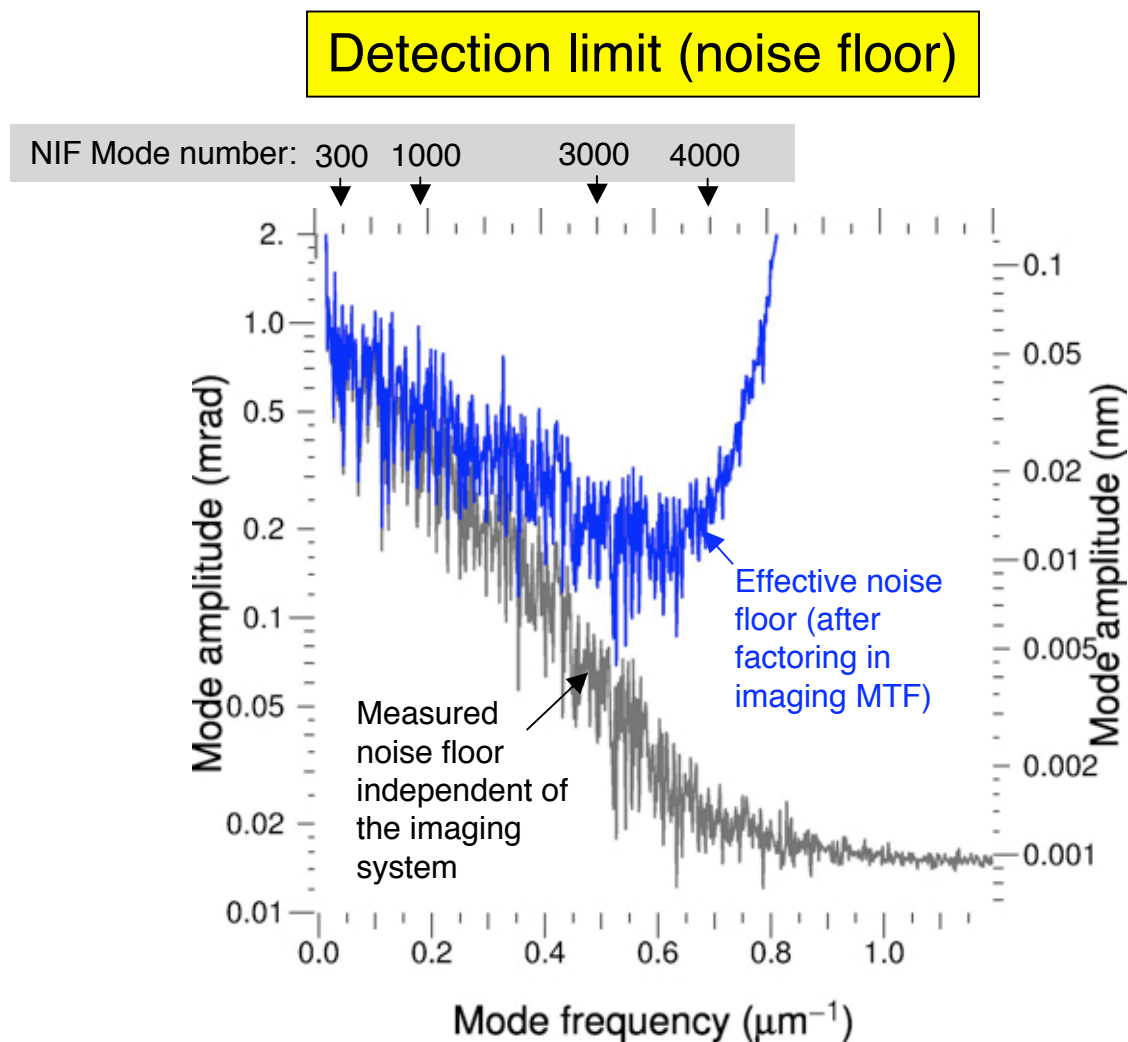
- [1] L. Barker & R. Hollenbach, J. Appl. Phys. **41**, 4208, (1970); J. Appl. Phys. **43**, 4669 (1972)
- [2] W. Hemsing, Rev. Sci. Instrum. **50**, 73 (1979)
- [3]* D. J. Erskine & N.C. Holmes, Nature **377**, 317 (1995)

The interferometer system records 4 frames simultaneously with 90 degree phase differences

- Diffraction-limited f/3 image relay system, 800 μm field of view
- System is implemented at OMEGA and known as the OHRV: “OMEGA High Resolution Velocimeter System”
- Incorporates a 1 mJ, 395 nm, ~ 2 ps laser source
- Streak camera for obtaining shock breakout & probe timing data



Detection limit (noise floor) of the system meets the NIF requirements

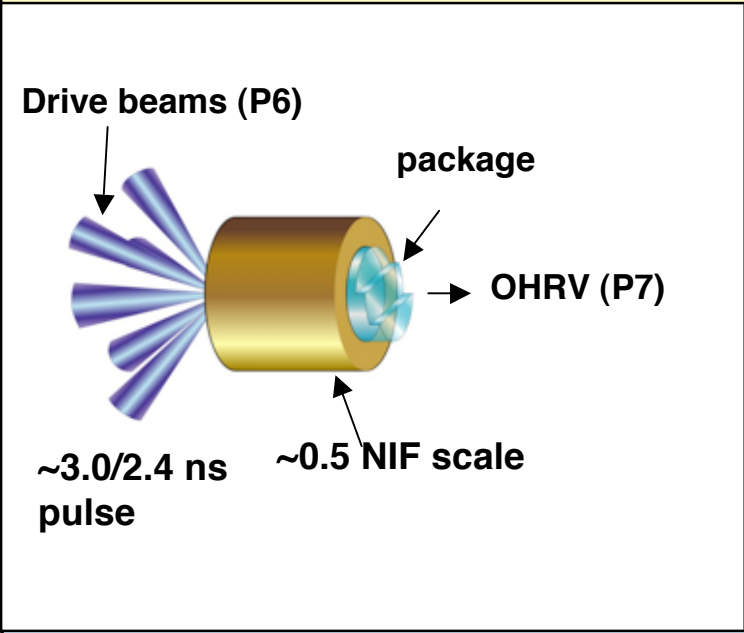


A platform for testing NIF ablator materials has been developed and fielded on OMEGA

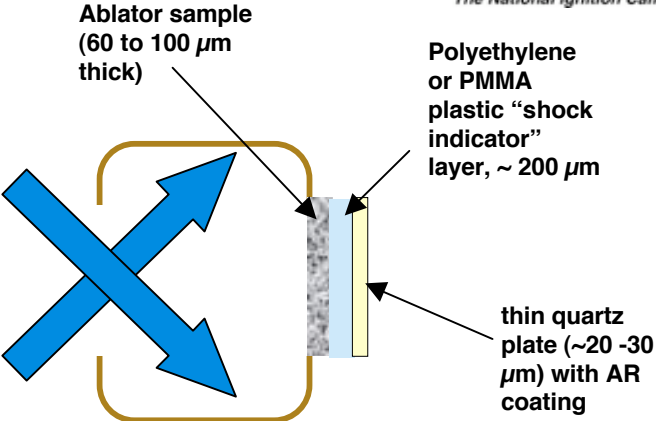


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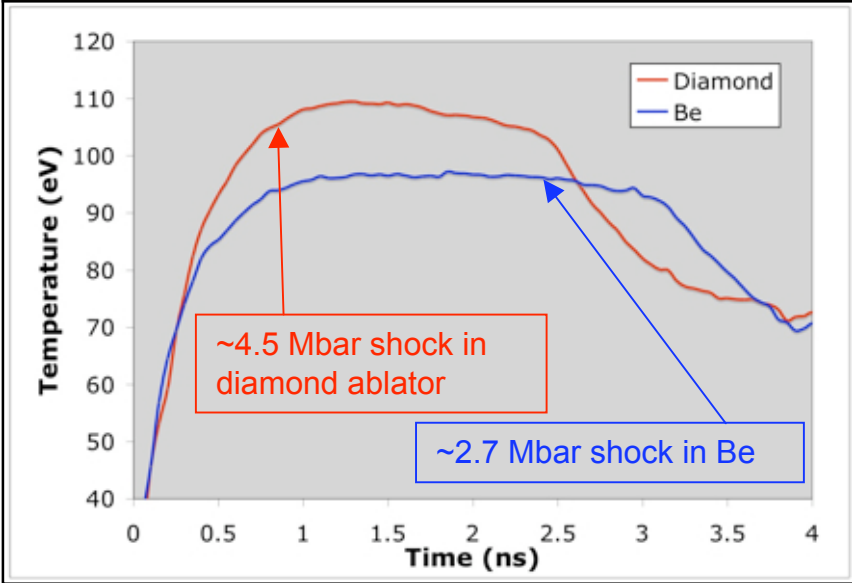
Omega Experiment for OHRV platform characterization



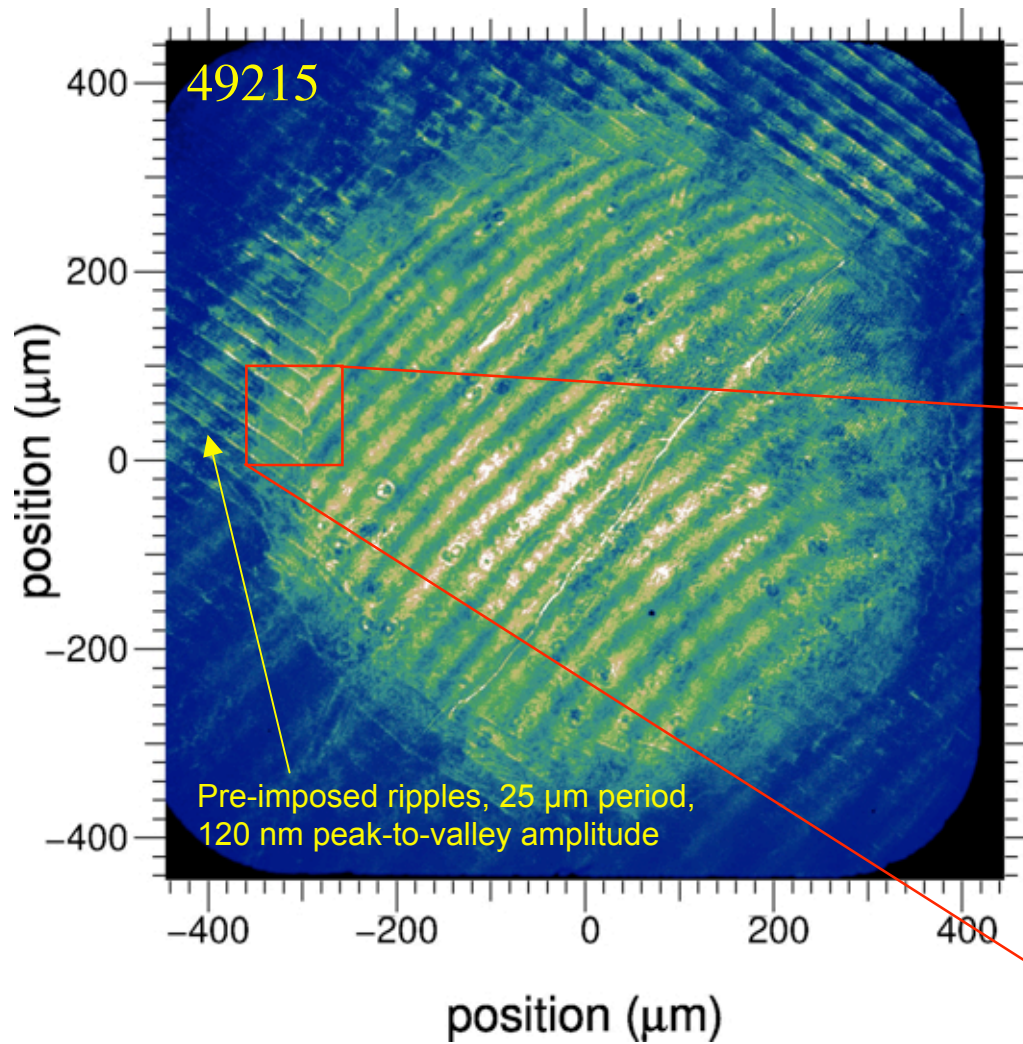
- Hohlraum size scaled from NIF to match Omega power
- Laser intensity & fraction of wall illuminated same as NIF



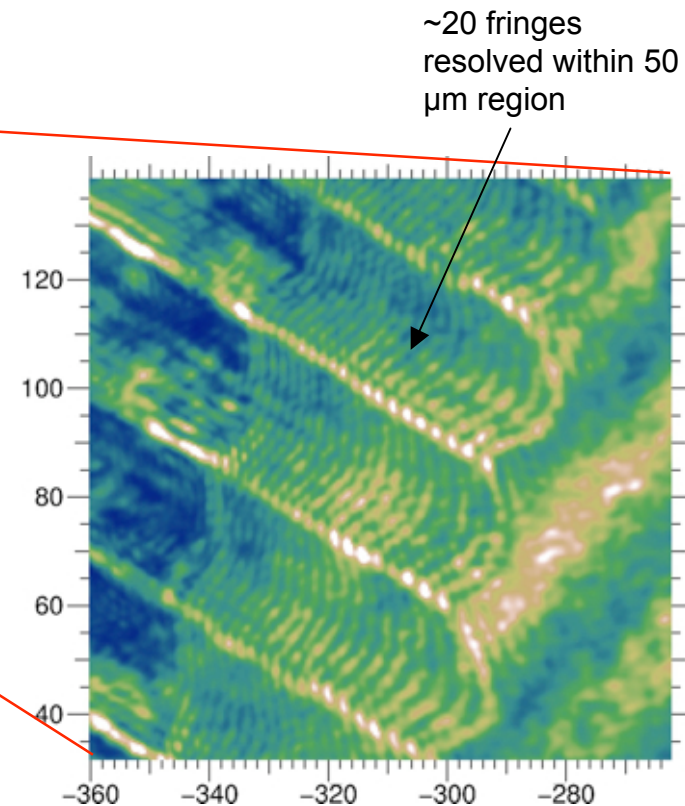
DANTE drive measurement



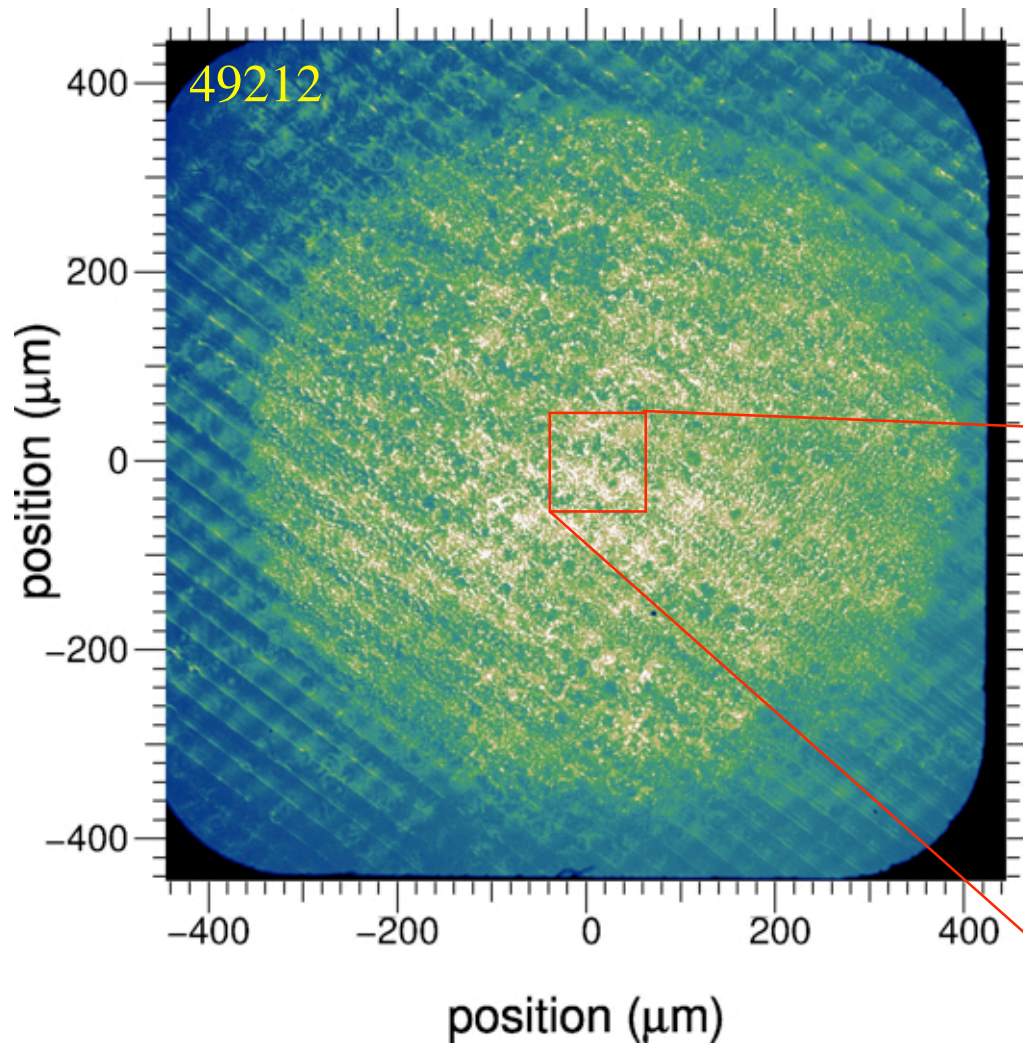
Example: Be(1%Cu) sample with pre-imposed ripples probed ~ 200 ps after shock breakout



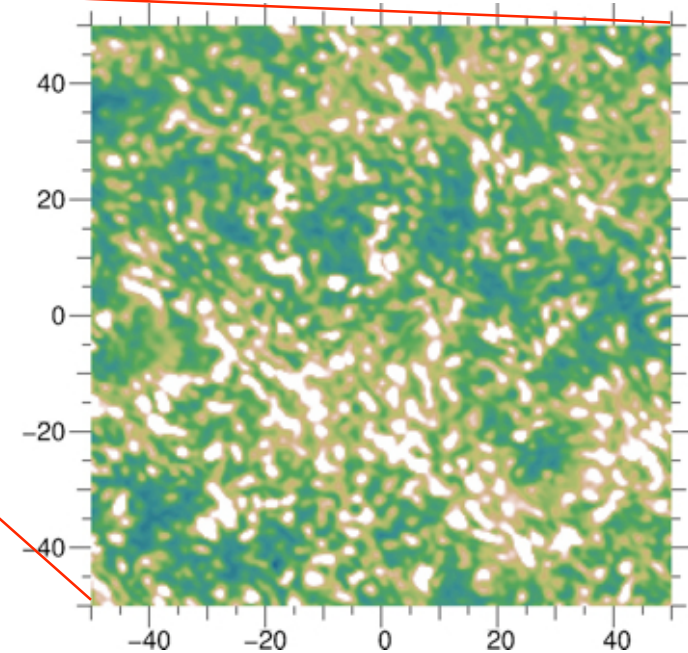
- Details down to $\sim 2 \mu\text{m}$ spatial scales can be resolved within the $800 \mu\text{m} \times 800 \mu\text{m}$ field of view



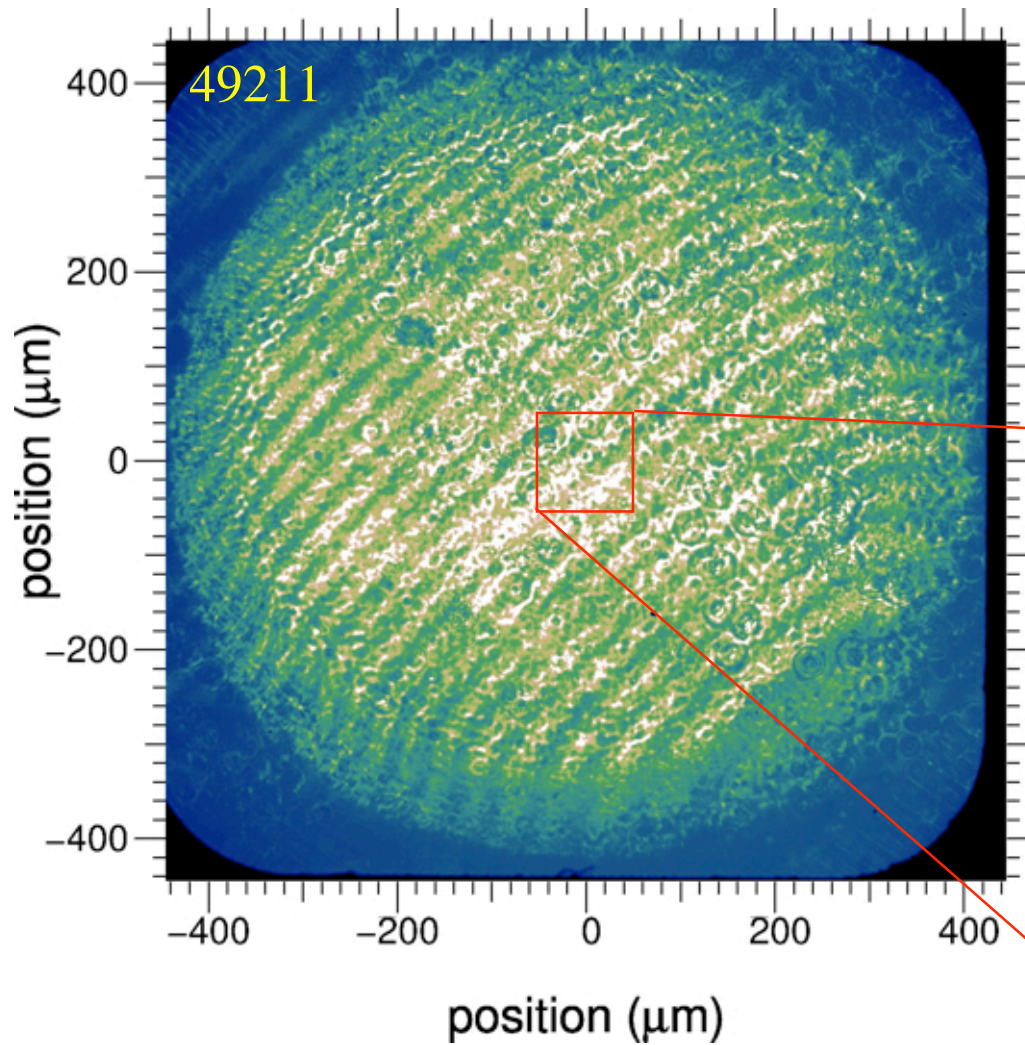
Example: nano-crystalline diamond with pre-imposed ripples probed ~ 50 ps after shock breakout



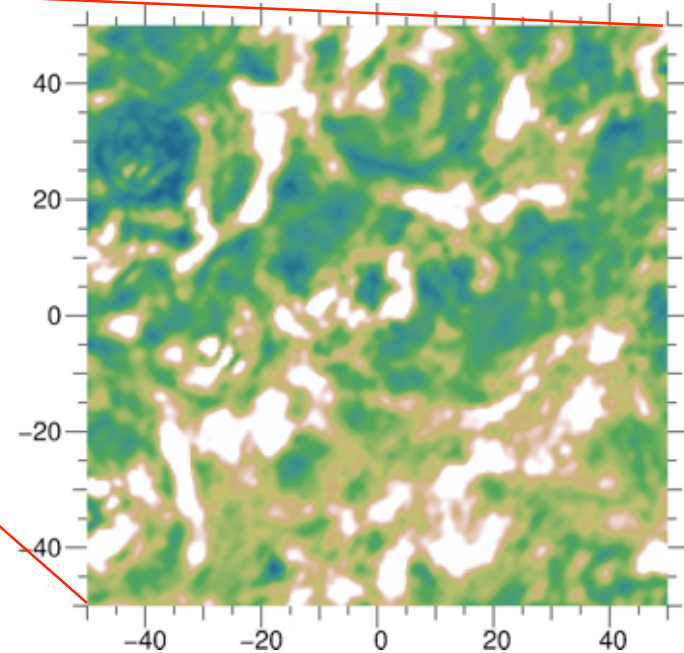
- Significant spatial structure is evident at the smallest resolvable sizes ($\sim 2 \mu\text{m}$)
- Extraction of the phase information (velocity fluctuation amplitudes) is in progress



Example: nano-crystalline diamond with pre-imposed ripples probed ~ 950 ps after shock breakout

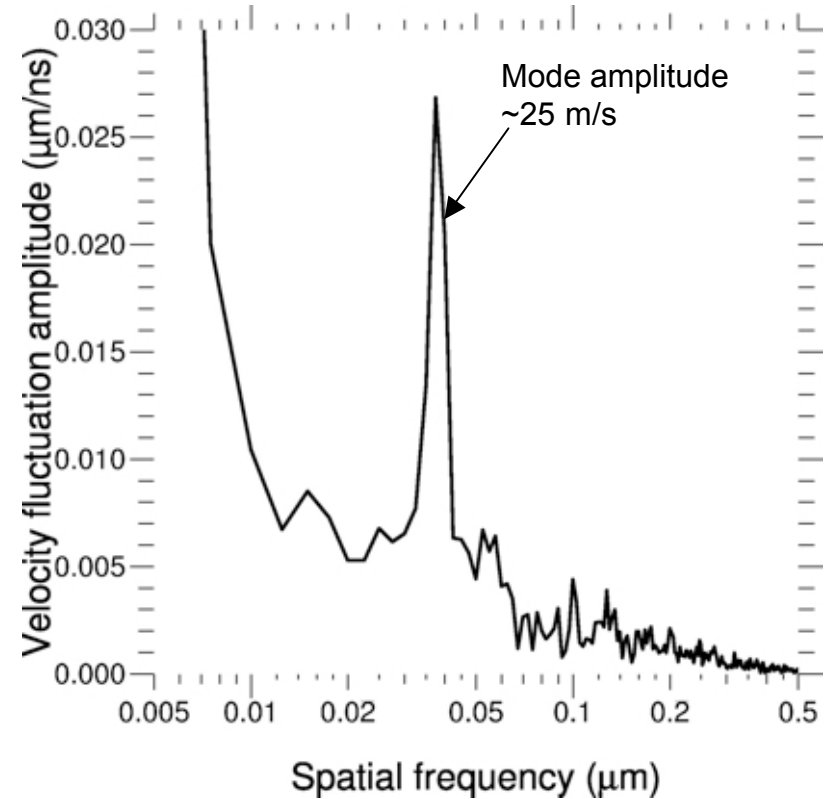
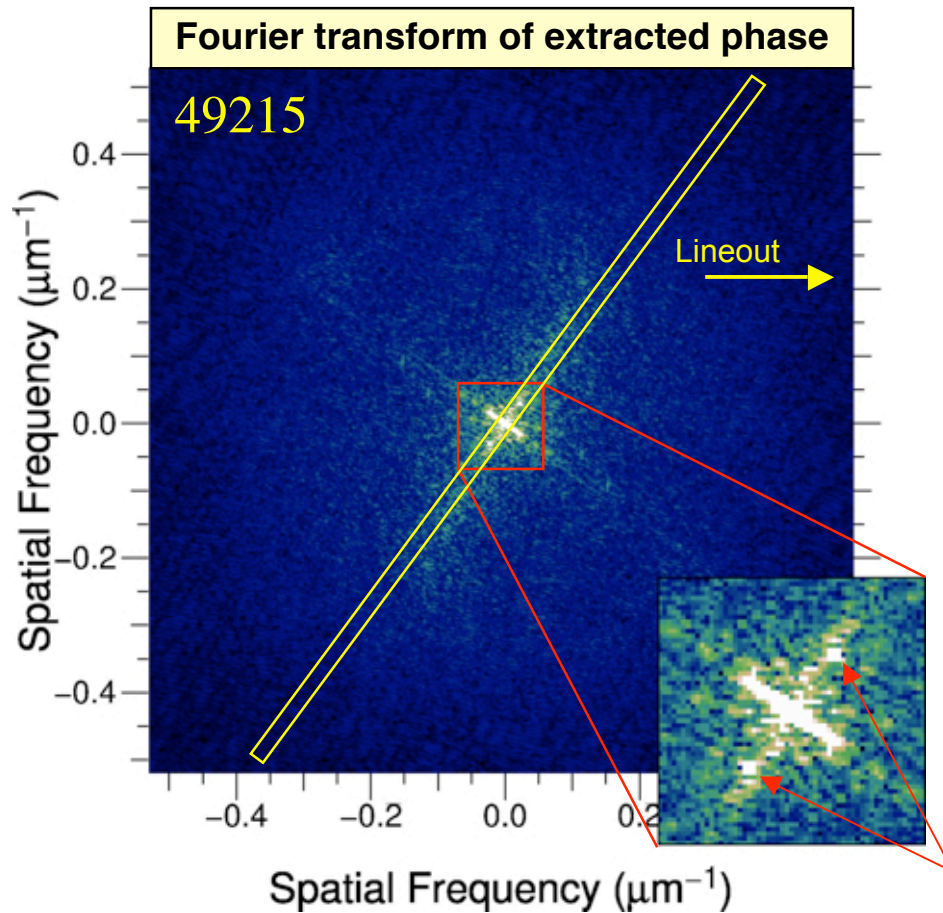


- Shock has propagated ~ 16 μm into the plastic
- Small scale modulations, $L < 10 \mu\text{m}$ have damped out



The pre-imposed ripple in 49215 is detected in the spatial frequency spectrum

- Observed ripple mode amplitude ~ 25 m/s compared to a noise floor of ~ 1 m/s per mode



These peaks in the 2D spectrum originate from the $25 \mu\text{m}$ wavelength pre-imposed ripple

Acknowledgments



The National Ignition Campaign

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- OMEGA operations staff

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- Dana Hargrove
- Glenn Jones
- Zack Sober

Summary

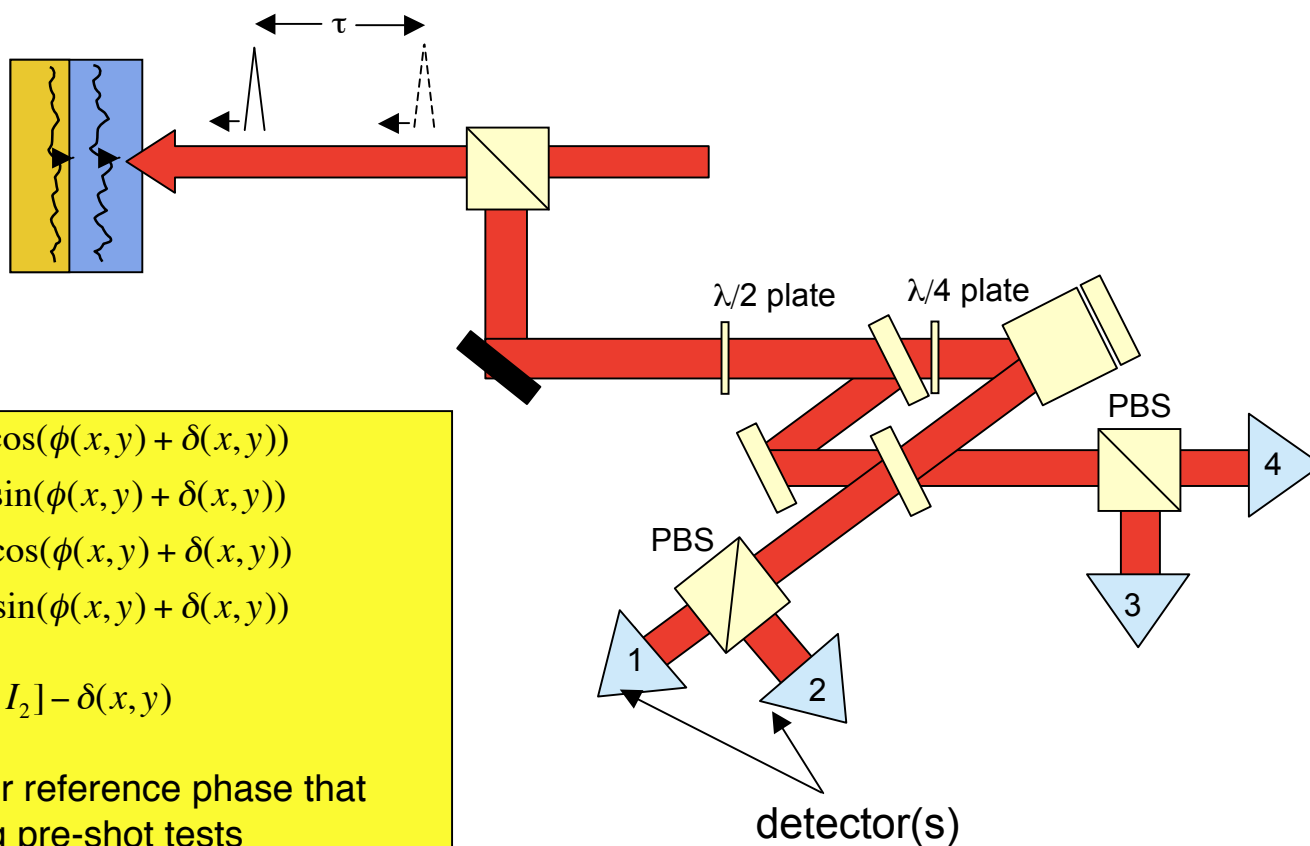
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Extras



A quadrature readout system is used to extract the phase

- Standard method for point VISARs used at other high pressure facilities
- Accurate phase extract down to single resolution element level



$$I_1(x, y) = B(x, y) + A(x, y) \cos(\phi(x, y) + \delta(x, y))$$

$$I_2(x, y) = B(x, y) - A(x, y) \sin(\phi(x, y) + \delta(x, y))$$

$$I_3(x, y) = B(x, y) - A(x, y) \cos(\phi(x, y) + \delta(x, y))$$

$$I_4(x, y) = B(x, y) + A(x, y) \sin(\phi(x, y) + \delta(x, y))$$

$$\phi(x, y) = \arctan[I_1 - I_3, I_4 - I_2] - \delta(x, y)$$

$\delta(x, y)$ is a background or reference phase that can be measured during pre-shot tests

The interference pattern produces a two-dimensional measurement of the velocity field just like a conventional VISAR

- Position of target (shock front) surface given by

$$Z(x, y, t) = - \int_{t_0}^t u(x, y, t) dt$$

— here t_0 is the time of shock breakout into the D_2 fluid, $u(x, y, t)$ describes the velocity of the shock front

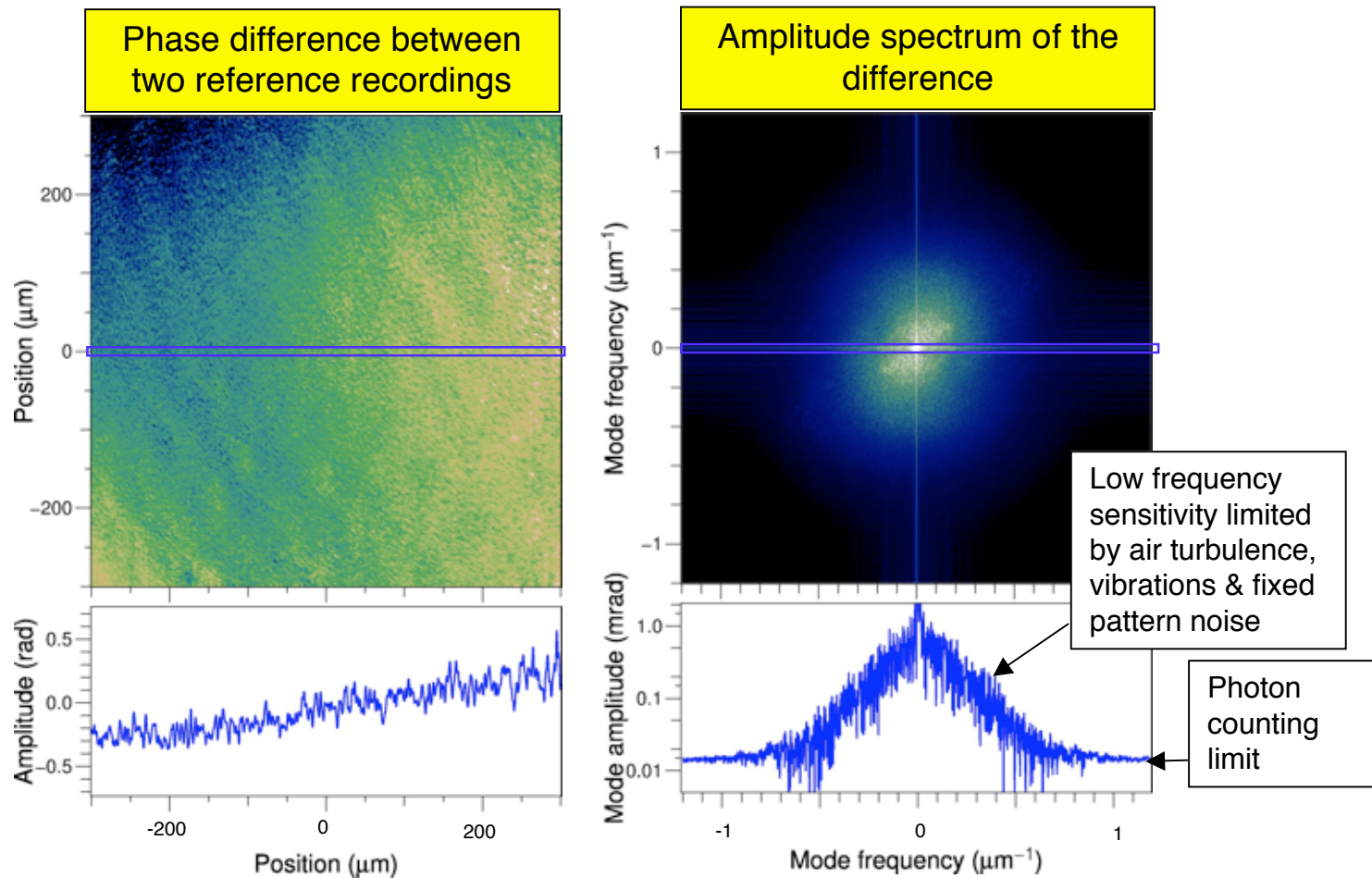
- By construction all fixed path delays cancel out: we set pulse 1 to interrogate the target at time t , pulse 2 at time $t+\tau$
- Net optical path delay:

$$\left. \begin{aligned} \Delta Z(x, y, t) &= - \int_{t_0}^{t+\tau} u(x, y, t) dt + \int_{t_0}^t u(x, y, t) dt \\ &= - \int_t^{t+\tau} u(x, y, t) dt \\ &= -\tau \langle u(x, y, t + \tau/2) \rangle \Big|_{\tau} \end{aligned} \right\} \Rightarrow \begin{aligned} \phi(x, y, t) &= 2nk(1 + \delta)\Delta Z(x, y, t) \\ &= -\frac{4\pi n}{\lambda}(1 + \delta)\Delta Z(x, y, t) \\ &= -\frac{4\pi n\tau}{\lambda}(1 + \delta)\langle u(x, y, t + \tau/2) \rangle \Big|_{\tau} \end{aligned}$$

- Observed phase is proportional to a moving average over time τ of the velocity field, centred at time $t+\tau/2$
- This is identical with the standard VISAR formula relating phase to velocity

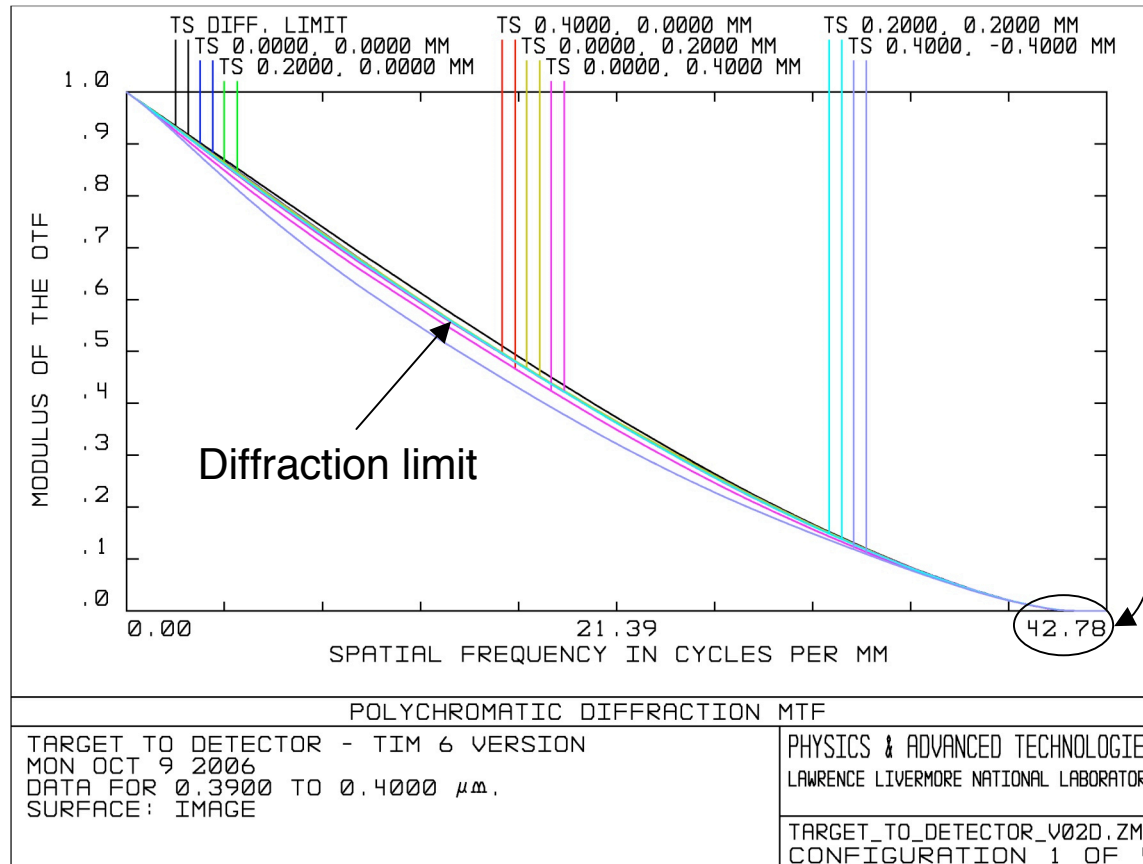
Determination the detection limit

- Record several blank interferograms and extract phase (reference phase maps)
- Subtract any two of the reference maps, difference reveals baseline noise level
- Apply FFT to evaluate noise spectrum



Spatial resolution of the OHRV system

- Design is modeled in ZEMAX and has been ray-traced from the target to the detector through the interferometer
- The design has been optimized to produce a diffraction-limited image at F/3 over the 800 μm x 800 μm field of view



Note: Calculation refers to image plane, multiply scale by 20 (system magnification) to get object plane response